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HEAT SUPPLY PLANNING IN THE CONDITIONS OF DEVELOPMENT OF ENERGY-EFFICIENT TECHNOLOGIES **IN CONSTRUCTION**

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4DH **4th Generation District Heating Technologies and Systems**

HEAT SUPPLY SYSTEMS IN RUSSIA

Russia has extensive co-generated heat and electricity system. More than one-half of electricity is co-generated with heat.

NUMBER OF CHP AND HEAT-ONLY BOILER PLANTS IN RUSSIA:

- 567 CHP
- 73511 heat-only plants (only 3392 of them with heat capacity more than 23 MW)

HEAT ENERGY PRODUCTION IN RUSSIA (2012 year):

- 709 million MWh by CHP
- 769 million MWh by heat-only plants with heat capacity more than 23 MW
- 209 million MWh by heat-only plants with heat capacity less than 23 MW
- 405 million MWh by individual sources
- 116 million MWh by other

The length of DH pipes - 169525 km.

HEAT ENERGY PRODUCTION AND CONSUMPTION IN RUSSIA

Source: the Energy strategy of Russia until 2035

REQUIREMENTS TO THE HEAT RESISTANCE FOR A BUILDING

 According to the Construction Norms and Regulations 23-02-2003 "THERMAL PERFORMANCE OF THE BUILDINGS" were approved different requirements for heat resistance for buildings constructed before the year 2000 and after.

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The Value of standardized specific heat energy consumption for heating an apartment in five large cities of Russia, Wh/(m²∙degree-day)

CLASSES OF ENERGY EFFICIENCY FOR BUILDINGS

HEAT DENSITY MAPS

Heat density map after adaptation of buildings

Existing heat density map

to requirements

<20 MW/km² >60 MW/km² 20-40 MW/km² 40-60 MW/km²

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ENERGY PLANNING PROBLEMS

1. Territory zoning. It is territory division into zones of the district heating (DH) and individual heating.

2. Justification of optimum levels of district heating and concentration of heat sources capacities.

Regulatory legal acts:

- 1. The Federal law № 190-FZ *On heat supply* (27.07.2010, ed. by 02.03.2014).
- 2. The Governmental order № 154 «*On requirements to heat supply schemes, the order of their development and approval*» (22.02.2012)
- 3. The Construction Norms and Regulations 11-04-2003 «*Guidelines on procedure of development, agreement upon, assessment and approval of town-planning documentation. Basic principles for urban planning and design (instruction)*» (The project of detailed planning)

HEAT SUPPLY PLANNING

The technique* allows to plan heat sources locations and a zone of their coverage when developing heat supply schemes.

Criteria for limitation of systems scale are:

heat density q_s

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• linear heat density q

1. V.A. Stennikov, E.E. Iakimetc, S.V. Zharkov. Optimal planning of the urban heat supply // Industrial power *engineering – 2013, №4. P. 9-15.*

Technologies and Systems

2. E. Iakimetc, V. Stennikov. Optimization methods of heat supply systems' scales// Proceedings from the 14th International Symposium on District Heating and Cooling, 6-10 September, Stockholm, SWEDEN. P. 526-529, 2014.

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FEATURES OF REGULATION CRITERIA **DEFINITION**

We take into account:

- 1. Different climatic conditions in the country.
- 2. The scale of built-up areas of settlements.
- 3. Economic conditions and characteristics of the territory.
- 4. Features of energy systems.

STANDARD VALUE OF HEAT DENSITY CRITERION DEFINITION

Standard value **q**_s is defined by comparison costs for DH system and for individual heating

Specific heat supply cost for DH

Equation for specific investment cost for pipeline construction subject to heat density.

р – pipeline operation costs and depreciation charges in shares from investment cost for pipeline construction; *α* – annuity;

m – approximation coefficient of numerical values of the specific cost of pipe laying with various values of heat density;

q^S – standard value of heat density (*MW/km²*).

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0.0 0.5 1.0 1.5 2.0 2.5 3.0 5 15 25 35 45 Total investment cost for the distribution network in area with 23 MW heat load (mln. EUR)

Heat density, MW/km²

IND rechnologies and Systems $Z_S^{DH}+Z_{HN} \leq Z^{IND}$. The childrengies and systems

S $z_{HN} = (p+\alpha) \cdot k_{HN} = (p+\alpha) \cdot \frac{m}{n}$ *q m*

STANDARD VALUE OF HEAT DENSITY CRITERION DEFINITION

 $Z_{S_n}^{DH} = \!\! \boldsymbol{C}_n \!+\! \boldsymbol{D}_n \cdot \boldsymbol{Q}_n, n \in \! N$. The deneration District Heating $\frac{DH}{S_n} = \!\! C_n \!+\! D_n \cdot \!\! \; Q_n, n \in \! N$ ath Generation District Heating $\sum_{\text{Technologies and Systems}}$

for heat sources Annual heat supply cost for DH $c_e \cdot \tau$ $\sum x_i \psi_i \cdot l_i$ $\cdot \tau \sum x_i \psi_i \cdot l_i$ $(\alpha + f) \cdot \sum_{i} k_i(d_i) \cdot l_i + \frac{\overline{i}}{362,7 \cdot \eta}$, $i \in I$ $Z_{HN} = (\alpha + f) \cdot \sum k_i(d_i) \cdot l_i + \frac{i}{\alpha + f}$, *i HN ⁱ ⁱ* $=(\alpha+f)\cdot\sum k_i(d_i)\cdot l_i+\frac{i}{\alpha}$, $i\in I$ $Q + I \cdot \sum K_i(Q_i) \cdot l_i + \frac{\cdots}{\cdots}$ i^{\perp} 26'

$$
\frac{e \cdot \tau \sum_{i} x_{i} \psi_{i} \cdot l_{i}}{362, 7 \cdot \eta}, \quad i \in I
$$

specific investment cost for $\longrightarrow k_i(d_i) = a_i + b_i d_i^{u_i}, i \in$ pipeline construction

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share of pipeline operation costs and $c_e \cdot \tau \cdot \sum_i x_i \psi_i$ depreciation charges from investment cost for pipeline construction

$$
k_i(d_i) = a_i + b_i d_i^{u_i}, i \in I
$$

and

$$
c_e \cdot \tau \cdot \sum x_i \psi_i
$$

i

 $i \in I$ $k_i(d_i)$ ^{, $i \in I$} $p = f + \frac{i}{2.62 \pi \sqrt{N} + i}$ *i* $i \mathcal{U}_i$ $e^{i\theta}$ $\sum_{i} \lambda_i \psi_i$ $\in I$ $\cdot \eta \cdot \sum k_i(d_i)$ $= f + \frac{i}{362,7 \cdot \eta \cdot \sum k_i(d_i)}, \quad i \in I$ $\sum x_i \psi_i$ $\frac{i}{362,7\cdot\eta\cdot\sum k_i(d_i)}, \quad i\in I$

f – depreciation charges, charges for maintenance and repairs of networks in shares from capital investments; Q_n – optimal heat output of the n-th heat source; a, b, u – coefficients in the equation of cost of a pipeline; *l* – route length; *τ*– number of hours of unit operation; *ce*– electricity cost; *η* – efficiency coefficient of pump; x_i – flow rate in the network sections ; ψ_i – the specific pressure drop in a network; *Dⁿ* , *Сⁿ* –coefficients of variable and constant costs for heat energy generation in a heat source.

STANDARD VALUE OF HEAT DENSITY CRITERION DEFINITION $1,16 \cdot m \cdot (p + \alpha)$ $m \cdot (p + \alpha)$ **4 DM** $\cdot m \cdot (p + \alpha)$ 4 D

 $=$ $\frac{1,10 \pi (p)}{q}$

 $f \circ f$ Ω *H*

Equation for standard value of heat density

Equation for existing value of heat density

production in decentralized sector;

capacity in district heating system.

S – the total land area of district.

HD – heat density for area,

DH \overline{s} – auditional specific inv

 $k_S^{\textit{IND}}$, $k_S^{\textit{DH}}$ – additional specific investment cost for

 b_f – specific consumption of fuel for heat energy

individual heating or for increasing of heat source

 c_f – cost of fuel;

$$
HD = \frac{\sum_{i}^{J} Q_{j}}{S}, j \in J
$$

 $q_s = \frac{1,10 \text{ m}}{G}$

s

 $0.001 \cdot \tau \cdot c_{f} \cdot b_{f} - \frac{c_{h}}{e^{nH}} - D_{n} + \alpha \cdot (k_{S}^{IND} - k_{Sn}^{DH})$

n

 $c_{f} \cdot b_{f} - \frac{c_{n}}{e^{DH}} - D_{n} + \alpha \cdot (k_{S}^{IND} -$

 $n = D + \alpha$, (k^{μ})

 D_H D_n α N_S N_{Sn})

 $\tau \cdot c_{\epsilon} \cdot b_{\epsilon}$ - $\frac{c_{\alpha}}{R_{\epsilon}r}$ - D_{α} + $\alpha \cdot (K_{\alpha} - K_{c_{\alpha}})$

 Q_n^{DH} \qquad \q

 $\cdot \tau \cdot c_{f} \cdot b_{f} - \frac{c_{n}}{e^{nH}} - D_{n} + \alpha \cdot (k_{S}^{IND} - k_{Sn}^{DH})$

 C_n **P** i. ex. (1 IND 1 DH)

 $DH \setminus$

Sn

IND I_r *DH*

 $D_n + \alpha \cdot (k_s^{IND} - k_{Sn}^{DH})$

 α , the state of α

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STANDARD VALUE OF LINEAR HEAT DENSITY CRITERION DEFINITION

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STANDARD VALUE OF LINEAR HEAT DENSITY CRITERION DEFINITION

 $q_l = \frac{11,33 \cdot c_e + c_p}{4} + \frac{1}{2}$

 $\frac{1}{\Delta t n} + \frac{1}{\mu^0}$ $\left(\begin{array}{cc} \Delta t \eta & \psi \end{array} \right)$

 $(11.55 \cdot c \cdot \tau \cdot w)$

Equation for standard value of linear heat density for main pipeline

Standard value of linear

Equation for existing value of linear heat density

The corresponding standard value of linear heat density with respect to electricity cost for other equal parameters

 $e^{-\mathcal{L} + \mathcal{L}}$

 $c_e \cdot \tau \cdot \psi$ 0,176*fb*

 $\Delta t \eta \qquad \qquad \psi^{0.27} \Delta t^{0.551} Q_{\scriptscriptstyle n}^{\;\;0.449} \; \; .$

 $11{,}55 \cdot c_{\scriptscriptstyle{e}} \cdot \tau \cdot \psi$ 0,176 fb $\tau \cdot Q_n^{\scriptscriptstyle{2\atop -4}$ 4th Generation Distriction

 $+\frac{0,170j\theta}{0.27-0.551-0.449}\left|\cdot\frac{\iota\cdot\mathcal{Q}_n}{\sigma}\right|$

 $\tau \cdot \psi$ $0,1/6fb$ $\tau \cdot Q_n$ Technologi

 η $\psi^{0.27} \Delta t^{0.35} Q_n$ C_n

 $=\left(\frac{11{,}55\cdot c_{e}\cdot \tau\cdot \psi}{\tau}+\frac{0{,}176fb}{\tau} \right{,} \frac{\tau\cdot Q_{n}}{\tau} \cdot \frac{\tau\cdot Q_{n}}{\tau} \cdot \frac{1}{\tau} \cdot \text{Riemann's function.}$

t η $\psi^{0.27}$

n

 $t^{0.551}Q_n^{0.449}$ C_n

 $\left|\cdot \frac{\sqrt{Q_n}}{C}\right|$ $\int \mathbf{C}_n$

 $\bigcap \ \tau \!\cdot \! O \!\!\bigg)^2$ - ^{4th Generation District Hear}

 $f b \qquad \quad \mid \; \tau \cdot Q_{\scriptscriptstyle n}^{\scriptscriptstyle \; 2} \quad \stackrel{\text{\tiny\rm 4th Generation District Hea}}{\scriptscriptstyle \text{\tiny\rm Technologies and System}}$

 $n \quad \bigg) \quad \biggarrow n$

 $\Delta t^{0.551} Q_n^{0.449}$ C_n

 L^{-} $\Delta t \eta$ $\psi^{0.27} \Delta t^{0.551} Q_n^{0.449}$ C_n

 $0.27 \wedge 0.551 \Omega^{0.449}$ Γ

n

 2 4th Generation District Heating

 $\displaystyle \mathcal{Q}_n^{-2}$ Ath Generation District Heating
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EXAMPLE

Individual heating

District heating

Pipelines from heat source-1 Pipelines from heat source-2

Variant 1 Variant 2 *qL*¹ 56*GJ* / *m* M

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EXAMPLE

Individual heating District heating Pipelines from heat source-1 **Variant 2** *qL*¹ 35*GJ* / *m* Variant 1 Pipelines from heat source-2 Pipelines from heat source-3

*qL*¹ 56*GJ* / *m*

2 **12** $q_{S1} = 35MW/km^2$ 2 \mathbb{Z} $q_{S1} = 23,5MW/km^2$

CONCLUSIONS

- Construction of building according to new standards of energy efficiency will reduce heat load density. It will influence on the efficiency of heating systems that is why there is a necessity of implementation of the energy planning considering new circumstances.
- \triangleright Several equations for determination of the standard values of heat density criteria for planning of heat supply are offered.
- Standard value of heat density criterion q_S for territory zoning mostly depends on: type and cost of used fuel, technical and economic characteristics of heat supply system, heat losses and climatic regional characteristics.
- \triangleright Standard value of linear heat density criterion q depends on: cost characteristics for heat sources, technical and economic characteristics of heat pipelines.
- \triangleright The Investigations of the influence of standards of heat load density (q_S, q_I) for urban planning proved that they define the rational determination of areas of district heating and individual heating, structure and scales of the heat supply systems.

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